Modelling D2D Systems using Visualyse Professional or Visualyse Interplanetary

Abstract: There is currently significant interest in the satellite and mobile industries in the potential to provide communication services from satellites direct to users with unmodified handsets. These types of systems are sometimes called direct-to-device (D2D), non-terrestrial networks (NTN) or supplementary coverage from space (SCS) and could involve a constellation of low Earth orbit satellites with large antennas that have the ability to provide such a service. But this brings in technical and regulatory challenges, from the type of services that can be provided, how to optimise coverage, capacity and throughput to the potential for interference to other services including terrestrial networks. This White Paper shows how these types of studies can be undertaken using the Visualyse Professional and Visualyse Interplanetary tools.

1. Background

Early in 2024, SpaceX launched six Starlink satellites with D2D capability, highlighting an acceleration of developments in the field of non-terrestrial networks. Previously, in 2023, AST SpaceMobile launched the BlueWalker 3 satellite which successfully connected with unmodified smartphones. Lynk Global is also developing its own D2D constellation. Simultaneously with the development of non-GSO constellations, work within 3GPP has incorporated support for NTN where issues to address include latency and Doppler compensation.

Whereas the engineering and standardisation tracks have made progress, the regulatory framework for D2D systems is still under development, with a new agenda item agreed at WRC-23. Some of the proposed D2D satellite networks are operating under a minimal "no interference, no protection" basis under Article 4.4 and there has been concern that this would not give terrestrial networks sufficient protection or certainty for the satellite network. Hence, the new agenda item 1.13 for WRC-27 to consider possible new allocations for mobile satellite service in parts of the UHF band taking into account the frequency arrangements used for terrestrial mobile networks.

In the US, SpaceX is working with T-Mobile to both provide a service which will handle both interference management and user contract including roaming rights. This approach requires close cooperation between satellite and terrestrial operators and there have been concerns that it might not provide sufficient protection for systems in adjacent bands or countries. For example, in the US, AT&T has raised concerns with the FCC at the potential for interference from SpaceX system into their operations in an adjacent frequency band. Other concerns have been raised, such as the FCC rejecting a plan for Starlink to operate at very low Earth orbits (VLEO) due to concerns about space traffic management with the International Space Station.

But why would SpaceX wish to operate at VLEO and what types of interference scenarios could there be? What are the critical factors involved in designing a D2D constellation and avoiding harmful interference into other systems?

These are complex scenarios to model, but Visualyse Professional and Visualyse Interplanetary are designed to model just these types of systems and those that a D2D constellation could share with, including terrestrial mobile, as discussed below.

2. Modelling a D2D Constellation

This section and the following one describes modelling of a D2D constellation and sharing with terrestrial services. All analysis was done using invented parameters and a SpaceX filing, and might not be representative of actual systems.

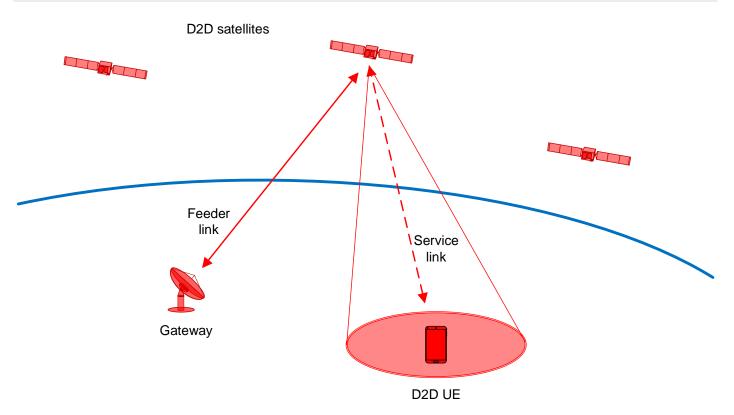
2.1. Overview

A D2D constellation consists of two main elements:

- **Space segment**: this involves a constellation of hundreds or even thousands of satellites in low Earth orbit. The number of satellites required will depend upon the required latency, link budget parameters and constellation sizing, with more satellites required for lower altitudes.
- **Ground segment**, including the user equipment (UEs) and gateways. In this White Paper we will concentrate on providing service to UEs, in particular unmodified mobile phone handsets.

The figure below shows these key elements:





2.2. Designing the Non-GSO Constellation

Two key attributes will impact the performance of a given non-GSO constellation to provide D2D services:

- 1) The coverage statistics of the constellation
- 2) The link budgets between the satellite and the UE.

These two are related and connected to the constellation configuration, and in particular the orbit altitude, with some of the benefits and costs as in the table below:

	Costs	Benefits
Lower altitude	More satellites = more capital expenditure Increased orbit drag / lower satellite lifetime	Lower latency Lower path length = better C/N for a given transmit power or less power required
Higher altitude	Higher latency Longer path length = worse C/N for a given transmit power or increased power required	Few satellites = lower capital expenditure Lower orbit drag / longer satellite lifetime

Some of the problems of lower C/N for higher altitude satellites can be overcome by more complicated and larger satellites, but with consequential cost implications.

Design of a non-GSO constellation involves trade-offs and usually some iteration to identify a set of candidates. Choice of preferred constellation is likely to require non-technical topics including finance and business related factors. The key is to be able to analyse candidates and identify the implications of using different orbits and technologies.

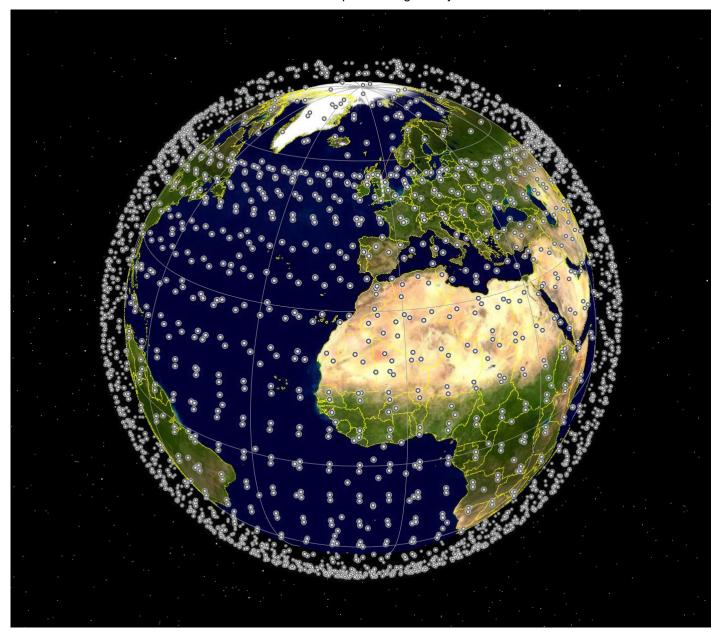
2.3. Coverage Analysis

The first stage is typically to undertake coverage analysis of a proposed non-GSO constellation. This identifies metrics such as:

• Number of satellites available to provide a service

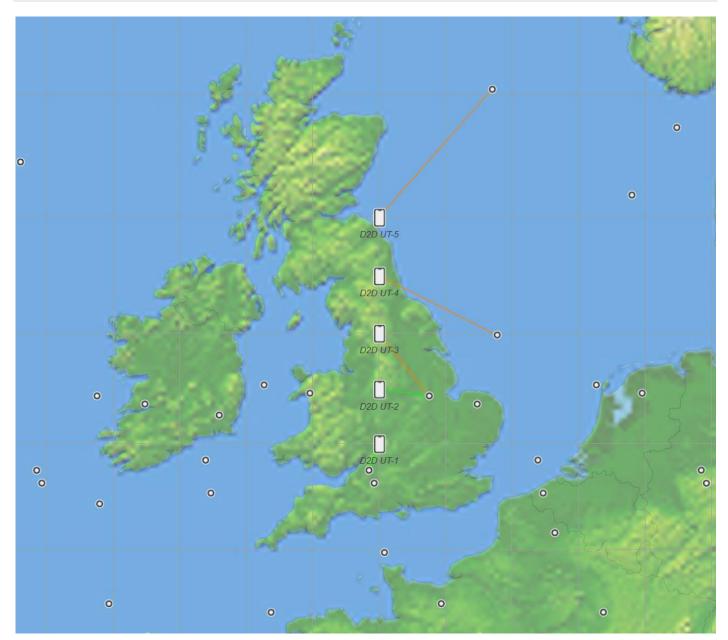
• Lowest elevation angle of highest (or second highest) elevation satellite over a time period such as a day. With constellations that do not maintain a repeating ground track, these will depend upon latitude only.

The constellation below was used to undertake an example coverage analysis:



This constellation, based upon a SpaceX filing, contains over 4,400 satellites at an altitude between 550 and 570 km, most at an inclination angle of around 53 degrees but with some polar planes.

Consider a set of test points in the UK, around the boundary of the inclination angle of the majority of the satellites:



For these test locations, it is possible to calculate the number of satellites above a minimum elevation angle and then the minimum elevation angle used if the UE were to select the highest available satellite at each time step. For D2D to UEs, it is useful to have as short a path length as possible, which means as high as possible an elevation angle so a minimum elevation angle of 50° was used in the statistics in the table below:

			Minimum highest
		Lowest number of	elevation angle used
D2D UE No.	D2D Latitude (deg N)	available satellites	(deg)
1	52	10	75.8
2	53	8	76.3
3	54	6	68.9
4	55	4	61.2
5	56	1	53.2

It can be seen that the best coverage is at around 52°N and 53°N, which is the inclination angle of the majority of the satellites of the constellation, but there is a significant reduction for higher latitudes.

This type of analysis can be extended to compare different constellation configurations and an extended range of metrics over a wider area.

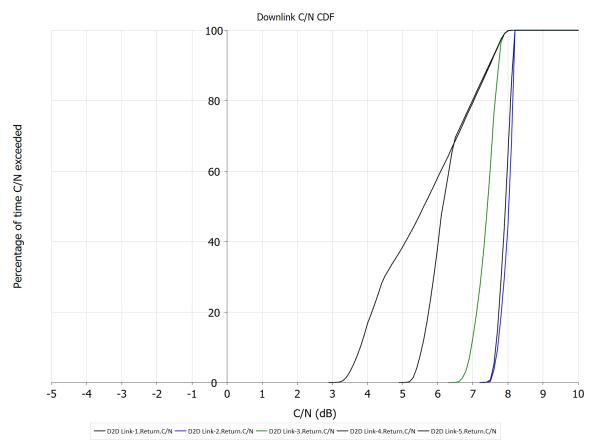
2.4. Link Budget Analysis

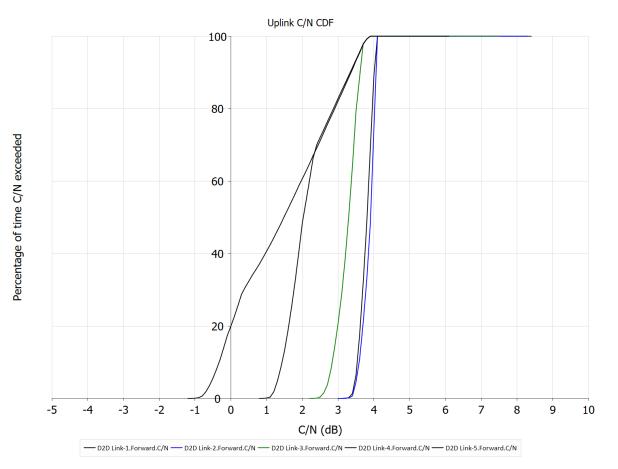
For these latitudes, link budgets can be created for both the uplink and downlink directions. The propagation models were assumed to be free space path loss plus the gaseous attenuation in Recommendation ITU-R P.676.

Parameters used for these systems are currently under development and it was necessary to make a number of simplifying assumptions to create the examples in this section as identified in the table below:

Direction	UL	DL
Frequency (MHz)	1900	2100
Bandwidth (MHz)	5	20
Tx power (dBW)	-8	10
Tx peak gain (dBi)	-3	31.1
Tx gain pattern	Isotropic	M.2101
Rx peak gain (dBi)	31.1	-3
Rx gain pattern	M.2101	Isotropic
Rx noise (K)	300	1500
Tr(C/N) (dB)	2.5	2.5

For these link parameters and the constellation described in the previous section, the C/Ns for the uplink (UL) and downlink (DL) were generated as in the following figures for one simulated day with a time step of 1 second:





The following can be seen:

- The downlink C/Ns are generally higher than the uplink C/Ns due to the availability of higher power at the satellite, despite the downlink bandwidth being wider than that for the uplink
- The C/N CDFs are better at the lower latitudes than higher as the path lengths to the satellite are lower.

In this case, in order to provide better coverage above around 56°N, there could be benefits in adjusting the non-GSO constellation. This could be done in a number of ways:

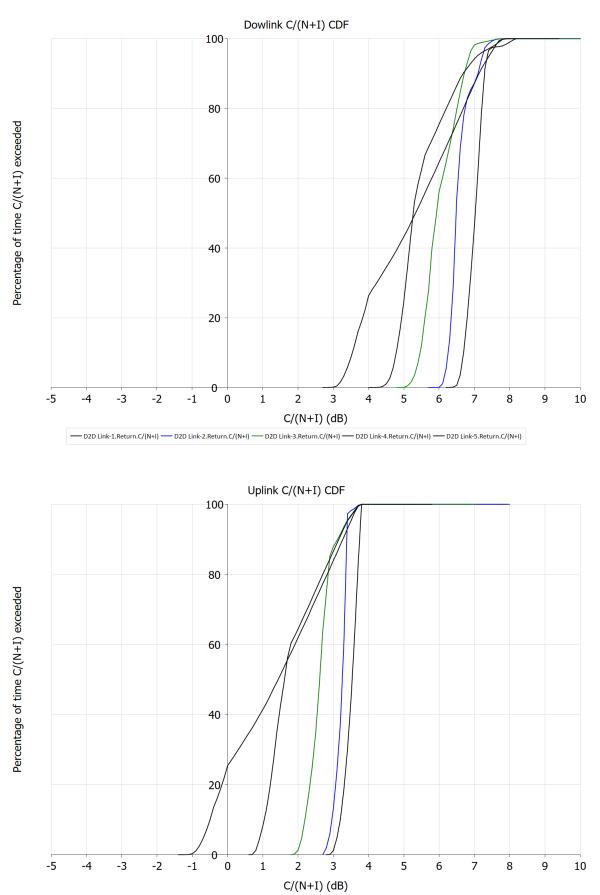
- Reduce the satellite altitude to reduce the free space path loss to the ground
- Increase the number of satellites visible at these latitudes.

2.5. D2D System Design

From this basic link budget study, more detailed analysis could be done, such as:

- Intra-system interference study, to identify how close together cells of UEs can operate co-frequency so that a single non-GSO satellite can point beams at both without causing harmful interference
- Capacity analysis, to identify the total capacity of the system, taking into account intra-system interference, power limits at the satellite, link engineering etc.

For the scenario above, each of the links were assumed to be co-frequency and causing interference into the others. The resulting C/(N+I) CDFs are shown below:



D2D Link-1.Forward.C/(N+I) — D2D Link-2.Forward.C/(N+I) — D2D Link-3.Forward.C/(N+I) — D2D Link-4.Forward.C/(N+I) — D2D Link-5.Forward.C/(N+I)

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Minor degradations in the C/N due to interference can be seen in the figures above and the table of derived values below:

Downlink direction	D2D Link-1	D2D Link-2	D2D Link-3	D2D Link-4	D2D Link-5
Worst C/N	7.2	7.2	6.3	4.9	3.0
Worst C/(N+I)	6.2	5.8	4.8	4.1	2.8
Percentage bad steps C/N	0.0	0.0	0.0	0.0	0.0
Percentage bad steps C/(N+I)	0.0	0.0	0.0	0.0	0.0
Throughput calculated using C/N	162265.0	163386.4	153809.4	137539.2	126851.4
Throughput calculated using C/N	148239.7	141189.8	133043.5	125707.1	122605.0

Uplink direction	D2D Link-1	D2D Link-2	D2D Link-3	D2D Link-4	D2D Link-5
Worst C/N	3.1	3.1	2.2	0.8	-1.2
Worst C/(N+I)	2.8	2.7	1.8	0.6	-1.3
Percentage bad steps C/N	0.0	0.0	0.4	72.1	71.2
Percentage bad steps C/(N+I)	0.0	0.0	34.9	75.6	73.0
Throughput calculated using C/N	100376.9	101349.7	93055.5	79035.3	69916.3
Throughput calculated using C/(N+I)	96377.4	92470.9	84646.7	74849.7	68728.5

More detailed analysis could identify the critical, minimum distance at which the system could no longer provide a service. However, the preferred distance is likely to greater than this, taking into account the balance between:

- Lower distance between co-frequency beams resulting in higher intra-system interference (and hence lower spectrum efficiency per beam) but allowing more beams (hence potentially greater spectrum efficiency overall)
- Greater distance between co-frequency beams resulting in lower intra-system interference (and hence higher spectrum efficiency per beam) but also fewer beams (hence potentially lower spectrum efficiency overall).

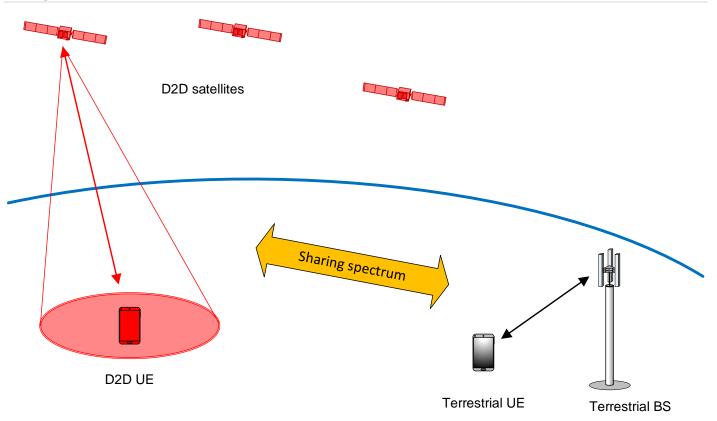
This analysis could be extended to derive throughput metrics for the constellation providing a service to a specific region, and hence alternative configurations considered, such as:

- Orbit height(s)
- Orbit inclination(s)
- Number of satellites
- Satellite antenna size / gain / number of elements
- Etc.

3. Sharing with Terrestrial Services

3.1. Scenario of Interest

Some D2D systems propose to use spectrum licensed to terrestrial mobile systems. This could lead to co-frequency spectrum sharing, as in the figure below:



One question would be the mode of operation used by each system, which could be:

- Frequency division duplex (FDD), same direction used by the two systems
- FDD, opposite directions used by the two systems
- Time division duplex (TDD) by both systems at the same time
- ... or some combination of FDD and TDD between the two systems.

All of these options could be considered and modelled in the Visualyse suite of tools.

In the sections below we'll consider the FDD (same direction) case. It can be seen there are a number of interference paths to consider:

Uplink:	1a. From D2D UE into terrestrial BS	(terrestrial path)
	1b. From terrestrial UE into D2D satellite	(Earth-to-space path)
Downlink:	2a. From D2D satellite into terrestrial UE	(space-to-Earth path)
	2b. From terrestrial BS into D2D UE	(terrestrial path)

The propagation models used for the interference paths were selected based on path type:

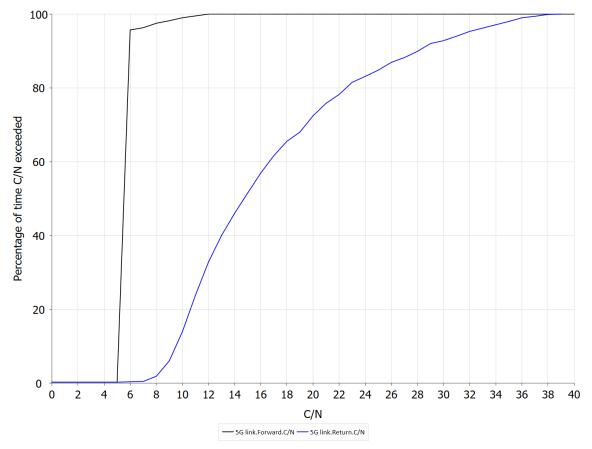
- Terrestrial paths: propagation model in Recommendation ITU-R P.2001 using smooth Earth diffraction.
- Space-to-Earth/Earth-to-space: free space path loss plus gaseous attenuation from Recommendation ITU-R P.676.

3.2. Modelling the Terrestrial Mobile System

Initially, let's consider just a single terrestrial mobile cell with the following simplified characteristics:

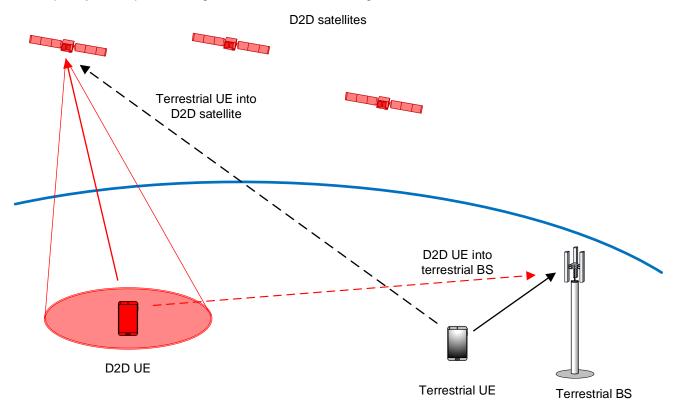
Direction	UL	DL
Frequency (MHz)	1900	2100
Bandwidth (MHz)	20	20
Power control	Yes	No
Max Tx power (dBW)	-7	-20
Tx peak gain (dBi)	0	17
Tx gain pattern	Isotropic	Parabolic
Rx peak gain (dBi)	17	0
Rx gain pattern	Parabolic	Isotropic
Rx noise (K)	2900	2900
Tr(C/N) (dB)	2.5	2.5

The propagation model for the wanted signal was Hata (open) with 4 dB of additional losses with the UE modelled at random across a service area of radius 500m. The resulting C/N CDFs are shown in the figure below.

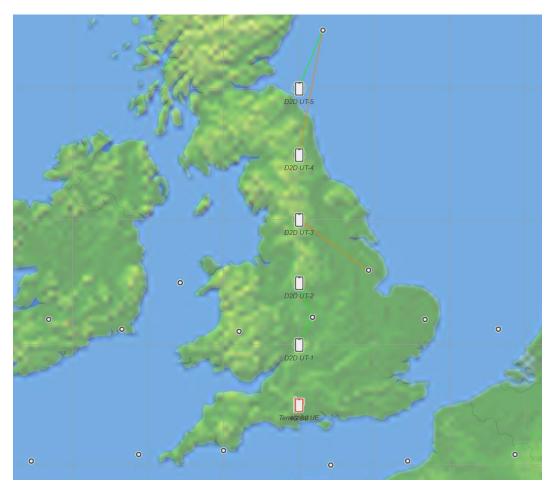


3.3. Uplink Sharing Scenario

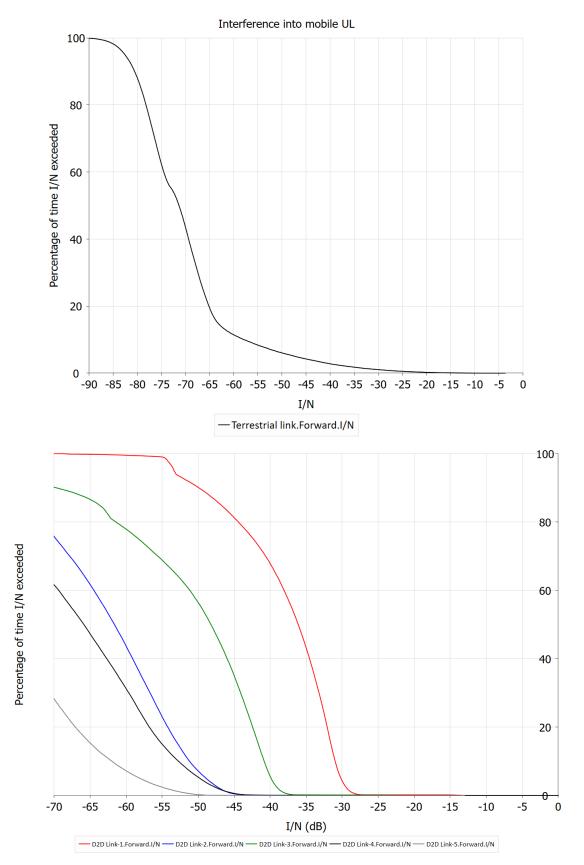
The co-frequency FDD uplink sharing scenario is shown in the figure below.



In the Visualyse simulation, all ground stations were located at the same longitude but separated by 1 degree in latitude as in the following figure.



The interference into the terrestrial mobile was the aggregate from all the D2D links. The analysis measured link performance using the $\{C/N, C/(N+I), I/N\}$ metrics. The I/N Complementary CDFs are shown in the figures below:



It can be seen that, in general, interference levels are low when the locations are separated by 1° of latitude (around 111.1 km). Interference into the D2D system decreased, the greater the separation distance to the mobile networks.

However:

- The interference into the D2D UL only considered a single terrestrial mobile when in reality there could be thousands if not millions transmitting co-frequency. Hence the I/N curve could be 30 or even 60 dB higher.
- There were times when the interference into the terrestrial system was above the Tr(I/N) = 6 dB due to anomalous propagation conditions. However, this was very rare, close to 0.001% of the time.

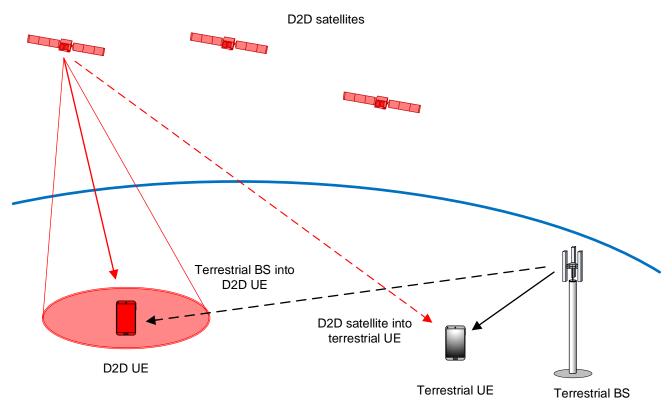
More detailed analyses could:

- Consider the aggregation of large numbers of terrestrial systems into satellite ULs (as in the section below).
- Consider the aggregation of multiple D2D UEs into a terrestrial system.

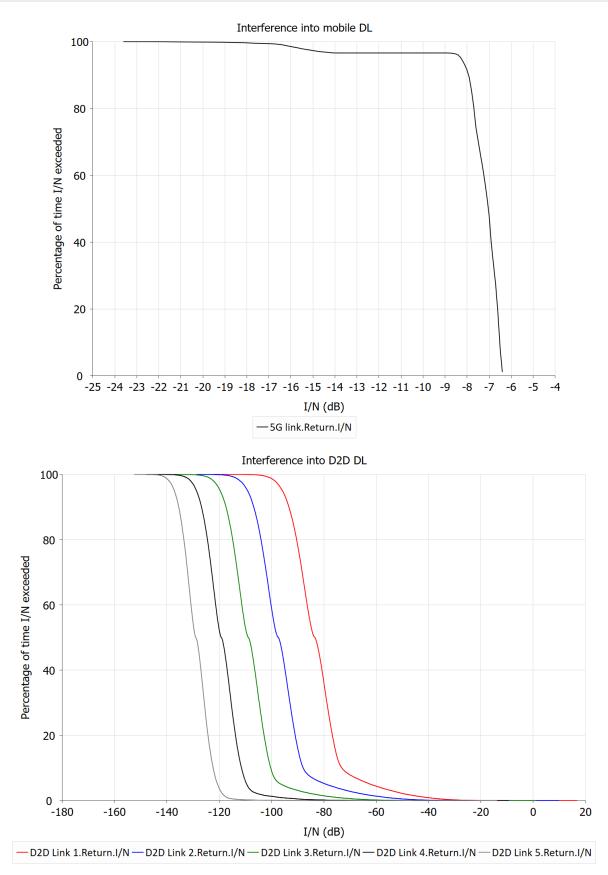
Such analysis would be required to identify the separation distances required to avoid harmful interference.

3.4. Downlink Sharing Scenario

The co-frequency FDD downlink sharing scenario is shown in the figure below.



A similar simulation file was used as for the UL case. The I/N plots are shown below.



It can be seen that, in general, interference levels are low when the locations are separated by 1° of latitude (around 111.1 km). Interference into the D2D system decreased, the greater the separation distance to the mobile networks.

Again, the interference into the D2D DL only considered a single terrestrial mobile when in reality there could be thousands if not millions transmitting co-frequency. However, there could be significant propagation loss due to terrain and clutter between the mobile network and the D2D handset.

More detailed analyses could:

- Consider the aggregation of large numbers of terrestrial systems into satellite DLs
- Consider the aggregation of multiple D2D DLs into a terrestrial system.

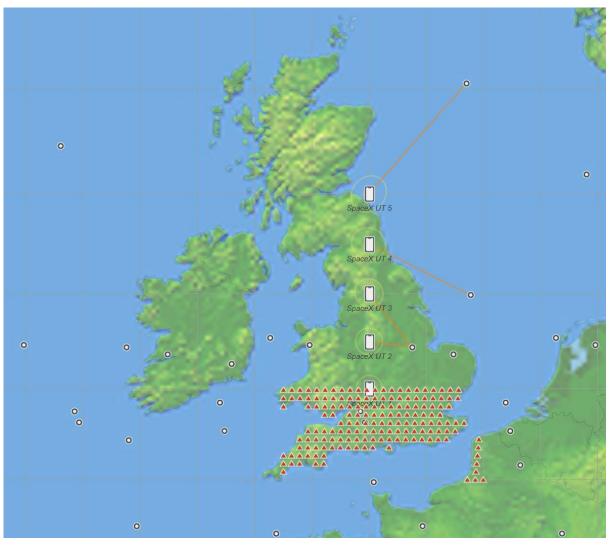
Such analysis would be required to identify the separation distances required to avoid harmful interference.

3.5. Modelling Aggregation

Aggregation can become a significant issue when there are large numbers of transmitters, such as the mobile UL into the D2D UL. In the analysis above, only a single mobile cell was considered, but there could be thousands if not millions. In these cases, it is necessary to undertake an analysis of aggregate interference.

One way to do that in Visualyse Professional is to deploy many stations over an area. As it is not possible to model the tens of thousands, if not millions individually, an approach is used whereby each station in Visualyse represents N actual stations and the power is increased by a factor = $10\log_{10}(N)$.

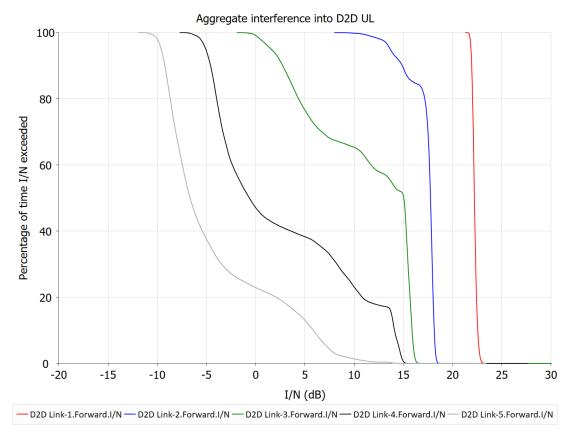
An example is shown in the simulation below:



Here, the service area wizard has been used to deploy a grid of 162 stations with separation 20 km across the land mass of England and Wales south of the lowest latitude D2D UE. To avoid the first of the D2D UEs being co-located with some of the terrestrial mobile stations, the array of D2D UEs was moved north 1°.

Each test station then represents all the actual UEs within a 20x20 = 400km² area. Assuming 1,000 UEs within that area, then the transmit power has to be increased by 30 dB. Assuming a power control adjustment factor of -3 dB, the aggregate EIRP per test station was set to 20 dBW. The propagation models were enhanced by use of the P.2108 Earth to space clutter model.

The resulting I/Ns are shown in the figure below.



It can be seen that the I/Ns are very high, in particular for those UEs close to the widespread mobile deployment. This could be analysed further, for example:

- The aggregate interference will be significantly affected by the gain pattern at the satellite and so alternatives could be considered e.g. continue to use the gain pattern in M.2101 but with adjusted parameter to reduce the beamwidth or different gain patterns (such as those in Recommendation ITU-R S.1528) etc.
- The aggregate interference decreases with separation distance, so greater distances could be considered.
- The mobile traffic levels also have a significant impact and would need further consideration. For example, the D2D UEs are likely to be deployed in regions with low terrestrial traffic, so there could be a gradual decrease in terrestrial mobile users rather than continuing at a high level until a fixed geographic line. In addition, time of day and other variations in loading could be included in the analysis.

4. Extending the Analysis

The analysis described above could be extended in wide variety of ways including:

- Consider a range of alternative parameters and configurations
- Consider alternative frequency bands
- Consider narrow-band and internet-of-things (IoT) constellations
- Consider alternative orbits types, including VLEO, LEO, MEO and GEO.
- Undertake sensitivity analysis
- Consider further aggregation cases, including those described above

• Use the "reference system" approach to modelling aggregate EIRP from an area, as described in our Technical Note:

https://download.transfinite.com/papers/Building_5G_Reference_Systems.pdf

- Undertaking analysis using C/N and C/(N+I) based metrics and derived parameters such as the increase in unavailability and loss of throughput due to interference
- Consider alternative scenarios and directions e.g. FDD reverse band, TDD mode etc.
- Considering alternative services to share with, including but not limited to broadcasting, fixed, space science and radio astronomy
- Considering non-co-frequency scenarios as well as co-frequency scenarios
- Undertaking more detailed Monte Carlo analysis that includes traffic factors
- Analysing the PFD generated by non-GSO constellations and considering the options for PFD limits (by elevation angle, along geographic borders etc.)
- Considering additional factors including Doppler (using Visualyse Interplanetary)
- Considering alternative regulatory solutions such as whether MSS spectrum should be used for the D2D UL but that MS spectrum could be used for the D2D DL?
- Etc.

No doubt these and many other factors will be considered during the WRC cycle!

As well as undertaking studies for WRC agenda items, there will be other requirements for studies, such as:

- Coordination studies: to coordinate a new D2D constellation with other existing filings
- National regulation: D2D system would require national licensing and if using spectrum licensed to terrestrial operators, will have to provide evidence that their operation would not cause them harmful interference
- Spectrum sharing methodologies: how to improve spectrum sharing so that a terrestrial operator could also use their spectrum for D2D systems most effectively.

With help of the Visualyse Professional and Visualyse Interplanetary suite of tools, those with an interest in this subject, whether a non-GSO satellite operator, a terrestrial operator or national regulatory administration, can achieve their regulatory objectives.

5. About Transfinite

We are one of the leading consultancy and simulation software companies in the field of radiocommunications. We develop and market the leading Visualyse products:

- Visualyse Professional
- Visualyse Interplanetary
- Visualyse GSO
- Visualyse EPFD and associated PFD Mask Generator Tool

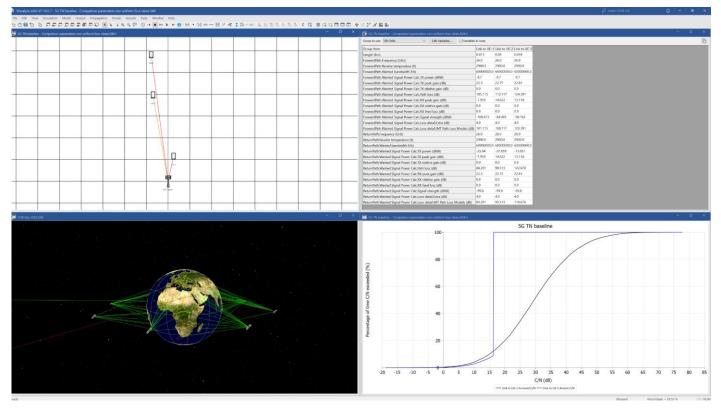
These are described further below.

5.1. Visualyse Professional

Visualyse Professional is a flexible study tool able to model a very wide range of radiocommunications systems, that can be used to analyse system performance including the impact of interference. Visualyse Professional can model transmit and receive stations located at fixed positions, mobile stations, aircraft, ships and also satellite systems including Earth stations, geostationary orbit, GSO satellites, non-GSO satellites and highly eccentric orbit (HEO) satellites.

It can be configured to analyse spectrum sharing scenarios using a wide range of methodologies, including static, input parameter variation, area, dynamic, Monte Caro and combinations such as area Monte Carlo.

Visualyse Professional includes a wide range of advanced features to enable it to analyse both co-frequency and nonco-frequency scenarios, the impact of terrain or clutter, the impact of traffic and complex handover strategies between satellites. These features allow it to model anything from a 5G network to a non-GSO mega-constellations such as SpaceX's Starlink or OneWeb. An example screenshot of Visualyse Professional is shown below:

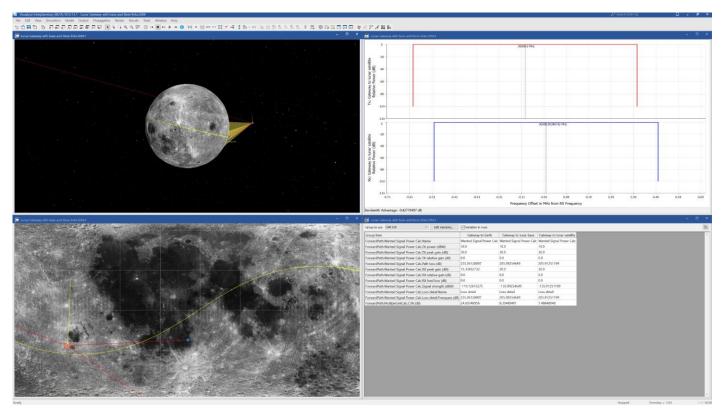


5.2. Visualyse Interplanetary

The objective of Visualyse Interplanetary is to extend the simulation ability of Visualyse Professional to allow:

- 1. Modelling of stations around other celestial bodies including the Moon and Mars
- 2. Enhance the geometric framework with a more detailed description of the Earth's shape and rotation characteristics.

An example screenshot of Visualyse Interplanetary is shown below:



5.3. Visualyse GSO

We have developed Visualyse GSO to support satellite coordination tasks, in particular for GSO satellites. It includes IFIC checker, detailed C/I calculation tool and integrates with ITU databases such as the SRS/IFIC and GIMS.

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SE-KA-43.6E NOR Www.01/1 C77.53.5, 555011 1017	INMARSAT-6-73E (Interferer) 4898G7W-		ର୍ 🛶 ଭ୍	Administration USA Notice ID 110500139	
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USCAE-25A USA Www.DT/T C67.12 % 2651/23 (MTP		KAD2 / G. KZGD. (KZGD.) (KAD. / C. (KZGD.) (KAD.) (C. (KZD.) (KZD		Orbital Location 60.00 dag E Orbital Separation 13.00 dag	
FM36-21.5E / Www.DT/T C 59 68 % 316922		17.95 18.15 18.3 18.5 18.7 19.05 20.3 ^{00,106/22} 20.7		Overlap Frequency 20,20000 21,20000 GHz	
AMS-CB-113E DR WestOTT (53.13 % 2001/23 MTT				* Coordination Arc Trigger	
MARLATIGE IN MARLATIGE MARLATIGE IN MARLATIGE MAR				Coordination Arc Exists Yes	
ASIABATAAA CHI WeeDTT CIBIDS 13541	1			Size of Acc 8.0 deg Inside Coordination Arc No	
F-SATING-JWW / Www.DTT (16.05 % 000022 000				v DT/T Trigger	
F-SATING-JE r WeekDTT (12/2 % 010022 CR				Interfering Group 122857030	
CHINASATD 87 SE CIN WWWDTT 5 1299 N 20102				Interfering Frequency 20.700000 GHz Emission 46596-7W	
F-SATING-152W / Www.DTIT (S.41 % 170022 CR				Satelike INMARSAT-6-73E	
AMS-87-13.8E BR Www.DTIT (9.41% 170015 MT				Satelite Location 73.00 deg E	
AMS-87-13.0E SR Www.DTT (9.14 % 170015 CTT AMS-87-13.0E SR Www.DTT (9.14 % 170015 CTT AMS-87-13.0E SR Www.DTT (9.14 % 170015 NTF	1	1795.005 (1)		Satelite Power -11.90 dBW/Hz V Satelite Off-axis Gain 43.00 dBi	
		20.7		Satelite On-axis Gain House Gain USD3	
		TICHE / TICL / TICHE / TICHE / T		Antenna Sidelobe Type Using peak gain	
	1			Satelite Peak Gain 43.00 dBI Satelite Off-axis Angle 2.29 deg	
✓ F-SATN10-84W F West0777 € 1.53 % 170622	USGOVSAT-10 (victim) KA 1		Show Priorities		
AMS-CE-113E ISR No Fireporte Courtee 28/10/15 NEE				Distance 35978.14 km	
ASIASATAAA CHN No Frequency Overlap 250123 (NTP					Report
lostr					CAP NUM SCR

The figure above shows the SRS/IFIC coordination trigger tool while the figure below shows the Visualyse GSO detailed coordination tool.

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	nto VENESAT-1 (downlink).dgso · D r Tools Help	Detailed Coordination								P Search (Ctrl+Q)	- 8
oup by: Beam		*) (-)(1ES	* • V Emission		*)(+					× 🗃 🗄 🗐 📟 👔	0.0
5AT-240 → VE				Max C, Max I OBW/12		-	Calculations		A A V Copy		
DOWNLINK					play All C		LINK BUDGETS	c	I	TK1 of USASAT-24Q → K2R of VENESAT-1	
DOWNLINK	Interform 1700 Victim	EIRP Gain BW	S Place Mattin ET 0		Threshold		v Satelite	VENESAT-1	USASAT-24Q		○ ①
1000		Law Gain Div	Pixes Pixer LS V			10000	Position deg	-78	-77	-	
	TYPICAL-K2 •			128/132	20.0	-4.006	Emission	36M0F3F	24K3G1W		
* ! IES 1	TYPICAL-K3 •			128/132	20.0	-4.006	Assignment GHz	11.725 M	11.718 M	TKI	
▶ ! VI	Emission: 28M8G7W •			54/55	20.0	-4.006	Polarisation	100601746	96823372	the at	
+ 1 V	Emission: 52K1G7W			4/4	20.0	-4.003	Group B/W MHz	50	30	1 12-52	
* 1 VI	Emission 1M21G7W .			414	20.0	-3.962	Allocated B/W MHz	36	0.0243	×	
	I Emission: 24K3G1W .			1/1	20.0	-3.962	Occupied B/W MHz	30	0.0203		
						Decostor of	* Tx Power dBW	1.7	1.9		
P.C.	Emission: 150KF3E •			1/1	20.0	-3.957	Pwr Density dBW/Hz	-73.07	-41.16		
P 1	Emission 48K6G1W •			1/1	20.0	-3.952	v Tx Gain dB	16 K2R	8 TK1		
1 I	Emission: SOKOF3E .			-121	20.0	-3.929	Boresight	N6.8303 W65.7465			
P I VI	Emission 6M95G7W .			9.9	20.0	-3.947	Radiation Pattern	REC-672 Ln25	From GIMS		83
NIV	Emission: 36M0F3F			57/60	20.0	-0 984	Beamwidth deg	1.5	6.69		Y
						a second second	Gmax dB	41	28		
	TYPICAL-K1 •			64/100	20.0	6.019	Angle deg	2.14	4.1	· K2R	
VES TYP	PICAL 3.7M ·			333/365	20.0	-4.006	Grel d8	-25	-20		
VES TYP	PICAL 3.0M ·			343/368	20.0	-4.003	 E3RP dBW Peak Density dBW/Hz 	17.7	9.9		
Beam Pair TK	2 - K2R •			2729/2868	20.0	-13 317	Offaxis Density dBW/Hz	-57.07	-33.16		1
-							Pathioss d8	205.07	205.06		
4	VENESAT 1					3 📀	v PFD dBW/m2/Hz	-219.31	-195.39		
Name	Gain Pattern Peak Gain	(dBI)		Id: 100520145 Admit	n: URG Pos	: -78.00 W	Spreading Loss dB	162.24	162.22		10
K2R	REC-672 Ln25 * 41.00						Elevation Angle deg	60.64	61.78		
AMS CIR	GEL KIR KAIR						* Rx Gain dB	52.6	30.45		
		_					ES Location	TYPICA	L 4.5M 7 W53.1470		
							Radiation Pattern	ITU-R S		ANALYSIS	
		1 Frepar	Ny Creat			1275 04	Beamwidth deg	0.42		ANALTSIS	
					Q		Gmax dBi	52.6		Dish See * GRID GRID CONTOURS DETAIL O	
					4-0	- 4	Angle deg	0.00	1.15		
			V V	T			Grel dB	0.00	-22.15	Constraints	
		11.700 - 1	2.200				Rx power dBW	-134.77	-164.7	Conseants	
1 = 100601746 1	Pri = M	Show assets for all bea	ms w				INTERFERENCE				
		28 DE3					⇒ 1 dBW	-133.79		VENESAT-1 (Victim)	
	TYPICAL 4.5M Typical	EARTH STATIONS	THIFFIONE	Name Designation	36M0F3 36M0F3		Adjustments dB	30.92		1 ☑ Gain Pattern set to ITU-R \$.580-6 for: TYPICAL 1.8M on Beam: K2R in Group: 100601742	
ю.	19pcal	P AT DOLD NO. ANALY I	EMISSIONS	Min Pwr (dBW)	-6.30	Par.	Bandwidth Adjustment dB Polarisation Loss dB	30.92		2 ✓ Boresight set to Lat 6.8, Long -65.7 for Beam: K2R on : VENESAT-1	
de (deg)	N/A	TYPICAL 1.8M	- 1M21G7W	Max Pwr (dBW)	1.70		Aggregation dB	0.00		3 Gain Pattern set to TRU-R 5.672-4 (Ln -25) for Beam: K2R on : VENESAT-1	
ude (deg)	N/A	TYPICAL 2.4M TYPICAL 3.0M	1M74G7W	Min Density (dBW/Hz)	-72,30		Aggregation Factor	1		Interference Cases	
iain (dBi)	52.60	TYPICAL 3.7M	- 6M95G7W	Max Density (dBW/Hz)	-61.30		C dBW	-134.77		4 Ø Polarisation set to 3.00 dB for Beam Pair: TK1→K2R and 25MZG1W into 28M8G7W	
width (deg)	0.42	TYPICAL 4.5M	28M8G7W				∀ C/I d8	-0.98		5 ☑ Aggregation Factor set to 1.40 for Beam Pair: TK1→K2R and 25M7G1W into 28M8G7W	
tion Pattern	REC-465 T	TYPICAL 2.6M	36M0F3F				Threshold dB	20			

Visualyse GSO can also consider non-GSO systems, for example during the import into the internal database as shown below:

lect Networks				
Source IFIC: srs2985_part	1of4 V IFIC	Network Type: Non-C	GSO v	
Apply Filters			Remember Filters	
Network Name v	ntains ~ falcon		- +	
•	5 Networks	1 Network Selected		
FALCONEYE FALCONEYE FALCONSAT FALCONSAT FALCONSAT FALCONSAT-6	N 119500123 A 116545113 N 117500266 A 110540767 A 119545091	FALCONEYE	N 119500123 srs2985_pa Θ	
V All		— All	OK Cance	1

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When in the internal database, a non-GSO system can then be considered during an IFIC check, in particular, to check for frequency overlap with other non-GSO systems.

5.4. Visualyse EPFD

Our Visualyse EPFD software is the leading implementation of the algorithm in Rec. ITU-R S.1503. It has been verified during testing with the ITU BR and can calculate:

- EPFD (Up)
- EPFD (Down)
- EPFD (IS)

It can also analyse both the Article 22 and Articles 9.7A and 9.7B cases.

It is available in two versions, one the ITU's "black-box" for pass/fail decisions and the other a product with graphical user interface that provides feedback on the calculation process and allows additional options to be modified.

The Visualyse EPFD software is also capable of undertaking analysis using the methodology in Resolution 770 and includes methods being proposed for inclusion in a revision to Recommendation ITU-R S.1503, such as the Alpha Table Methodology.

An additional tool, the PFD Mask Generator Tool is available to assist in the generation of PFD masks.

5.5. Training Courses

We also provide training courses in the use of our products including advanced training that can cover modelling of specific systems and scenarios, as non-GSO satellite coordination.

5.6. Consultancy Services

We can provide a wide range of consultancy services using our world-leading experts and software tools to rapidly generate solutions, including:

- Interference analysis and spectrum sharing studies
- Coordination support and meeting representation
- ITU-R and CEPT meeting representation and support
- Strategic consultancy to achieve regulatory goals.

5.7. Contact Us

More information about these products and services is available at our web site:

https://www.transfinite.com

If you have any questions or comments about this Newsletter or would like more information, please do not hesitate to contact us at:

info@transfinite.com